

DESCRIPTION

ANTENNA SWITCH MODULE

5 THIS APPLICATION IS A U.S. NATIONAL PHASE APPLICATION OF
PCT INTERNATIONAL APPLICATION PCT/JP2005/013031.

TECHNICAL FIELD

 The present invention relates to an antenna switch module
10 including an antenna switch which switches antennas, and a filter
which passes fundamental frequencies and has an attenuation
pole.

BACKGROUND ART

15 Fig. 12 shows a block diagram of a conventional
communication device including conventional antenna switch
module 80. Conventional antenna switch module 80 will be
described with Fig. 12. In Fig. 12, the communication device
includes antenna switch module 80, transmission part 41,
20 reception part 42, filter 83, antennas 44 and 45, and capacitors
C81 to C84.

 Conventional antenna switch module 80 includes antenna
switch circuit 87 and filter 86. Signals from transmission part
41 are inputted to filter 86 through capacitor 81. Filter 86
25 passes fundamental frequencies and removes unnecessary signals.
Signals outputted from filter 86 are emitted from antenna 44
or 45 selected by antenna switch circuit 87, after passing
through capacitor C83 or C84.

On the other hand, signals which are received by antenna 44 or 45 selected by antenna switch circuit 87 and then are passed through capacitor C83 or C84 are inputted to filter 83 through capacitor C82. Filter 83 removes unnecessary signals from the received signals and outputs them to reception part 42. Reception part 42 demodulates the signals from filter 83.

Filter 86 included in antenna switch module 80 will be described with reference to Figs. 13 to 16. Fig. 13 shows the structure of the filter for the conventional antenna switch module. In Fig. 13, capacitors C94 connected to the ground are open circuit to low frequency components and are short circuit to high frequency components. Inductor L94 connected in series with capacitors C94 are short circuit to low frequency components and are open circuit to high frequency components. Thus, the filter shown in Fig. 13 is a low pass filter, which passes low frequency components only.

The low pass filter shown in Fig. 13 has a large circuit size because rapid attenuation can be achieved only by a large number of stages. Alternatively, rapid attenuation can be achieved by a few number of stages when the constant of each element of this filter is determined in such a manner as to make the filter a Chebychev low pass filter. However, it is difficult for this filter to achieve wideband filtering at low loss because the filter has ripples in the passband. Another possible structure is achieved by the use of distributed constant lines. In this case, however, when a certain frequency is reached, inductive distributed constant lines are changed to capacitive distributed constant lines, whereas capacitive distributed constant lines are changed to inductive distributed constant

lines. The input impedance greatly changes depending on the frequency, thereby sometimes causing the filter to lose its function as a filter.

In view of this situation, a polarized low pass filter shown in Fig. 14 has been contrived. Fig. 14 shows the structure of this filter for the conventional antenna switch module. Fig. 15 shows frequency characteristics of this filter for the conventional antenna switch module. The principle of operation of the filter will be briefly described with Figs. 14 and 15.

Polarized low pass filter 90 includes LC series circuits 96, 98 and 99. As shown in Fig. 15, the attenuation band in the frequency characteristics of filter 90 has three poles: a first pole of 13.2 KHz; a second pole of 15.4 KHz and a third pole of 25.3 KHz. Here, for example, decreasing the resonant frequency of LC series circuit 98, that is, the second pole frequency can reduce the interval between the first pole and the second pole. Reducing the interval between these poles results in an increase in the amount of attenuation between the poles.

As a filter for the conventional antenna switch module, one example of the aforementioned polarized low pass filter is disclosed in Japanese Patent Unexamined Publication No. 61-77408.

Another known filter for an antenna switch module is a notch filter with little filtering loss. A notch low pass filter can be formed of a combination of a plurality of $1/4$ wavelength open stubs and $1/2$ wavelength terminated stubs. Fig. 16 shows frequency characteristics when antenna 44 or 45 is seen from transmission part 41 in a case where filter 86 of the conventional

antenna switch module is a notch filter. Fundamental frequencies are from $F1=4.9$ GHz to $F2=5.85$ GHz. Second harmonic frequencies are from $F3=9.8$ GHz to $F4=11.7$ GHz. Third harmonic frequencies are from $F5=14.7$ GHz to $F6=17.55$ GHz. The frequencies of the attenuation poles are set so as to attenuate the second and third harmonics.

In such a conventional structure, the second harmonic frequencies have small attenuation at other than the two attenuation poles $F3$ and $F4$, and the third harmonic frequencies have small attenuation at other than the two attenuation poles $F5$ and $F6$. In other words, the impedance when the output side of filter 86 is seen from the input side, and the impedance when the input side is seen from the output side both approach 50 ohms. On the other hand, impedance $Z813$ when terminal $T83$ connected with capacitor $C83$ is seen from terminal $T81$ of antenna switch circuit 87, which is connected with filter 86 is about 50 ohms at the fundamental frequencies. Impedance $Z842$ when terminal $T82$ connected with capacitor $C82$ is seen from terminal $T84$ connected with capacitor $C84$ is also about 50 ohms at the fundamental frequencies. On the other hand, impedance $Z814$ when terminal $T84$ is seen from terminal $T81$ and impedance $Z832$ when terminal $T82$ is seen from terminal $T83$ are open circuit. However, as the frequency gets higher, the capacity component and induction component of the package and terminals of the PIN diode become influential. This causes impedances $Z813$, $Z842$, $Z814$ and $Z832$ to change their values. More specifically, impedances $Z813$ and $Z842$ have values close to open circuit at the harmonic frequencies ranging from 4.9 GHz to 5.85 GHz, and impedances $Z814$ and $Z832$ have values close to 50 ohms. As a result, at the

harmonic frequencies, the impedance Z813 when filter 86 is seen from terminal T81, and impedance Z814 when antenna switch circuit 87 is seen from terminal T81 can be complex conjugates of each other. This may deteriorate the amount of attenuation at the
5 attenuation poles or cause a rebound phenomenon between the attenuation poles, thereby making it impossible to have enough attenuation.

SUMMARY OF THE INVENTION

10 The present invention provides an antenna switch module including a filter which can reduce filtering loss so as to achieve high attenuation in a wide band at harmonic frequencies.

The antenna switch module of the present invention includes the filter, an antenna switch circuit and an adjustment
15 line. The filter passes fundamental frequencies and has an attenuation pole. The antenna switch circuit switches antennas matching the fundamental frequencies. The adjustment line is connected between the filter and the antenna switch circuit, and adjusts properties of the fundamental frequencies at the
20 harmonic frequencies. When the filter and the antenna switch circuit are directly connected with each other at a connection point, the adjustment line prevents the impedance when the filter is seen from the connection point and the impedance when the antenna switch circuit is seen from the connection point from
25 becoming complex conjugates of each other at the harmonic frequencies.

This antenna switch module can easily reduce rebound components between the attenuation poles of the filter at the harmonic frequencies without degrading the amount of

attenuation at the attenuation poles, thereby fully attenuating the harmonic components without increasing the number of stages of the filter. For example, fundamental frequency signals amplified by a power amplifier in the front end module of a wireless LAN (Local Area Network) are passed at low loss, and the harmonic components generated by the power amplifier can be removed in a wide band at high attenuation.

BRIEF DESCRIPTION OF THE DRAWINGS

10 Fig. 1 is a block diagram showing the structure of a communication device including an antenna switch module of an embodiment of the present invention.

 Fig. 2 shows a first layer of the antenna switch module of the embodiment.

15 Fig. 3 shows a second layer of the antenna switch module of the embodiment.

 Fig. 4 shows a third layer of the antenna switch module of the embodiment.

20 Fig. 5 shows a fourth layer of the antenna switch module of the embodiment.

 Fig. 6 shows a fifth layer of the antenna switch module of the embodiment.

 Fig. 7 shows a sixth layer of the antenna switch module of the embodiment.

25 Fig. 8 shows the structure of an antenna switch circuit of the antenna switch module of the embodiment.

 Fig. 9 is an equivalent circuit diagram when a PIN diode as a component of the antenna switch circuit of the embodiment is "ON".

Fig. 10 is an equivalent circuit diagram when the PIN diode of the embodiment is "OFF".

Fig. 11 shows frequency characteristics of the antenna switch module of the embodiment.

5 Fig. 12 is a block diagram showing the structure of a communication device including a conventional antenna switch module.

Fig. 13 is a circuit diagram of a filter for the conventional antenna switch module.

10 Fig. 14 is a circuit diagram of another filter for the conventional antenna switch module.

Fig. 15 shows frequency characteristics of the filter for the conventional antenna switch module.

Fig. 16 shows frequency characteristics of the
15 conventional antenna switch module.

REFERENCE MARKS IN THE DRAWINGS

- 3, 7, 8 round conductor
- 4, 5A, 5B ground part
- 20 6A, 6B, 6C, 6D, 6E electrode
- 11A, 11B, 11C, 11D, 13A, 13B, 13C stripline
- 13D adjustment line
- 15 coupling line
- 30 antenna switch module
- 25 31, 43 filter
- 33 antenna switch circuit
- 35 directional coupler
- 41 transmission part
- 42 reception part

44, 45 antenna

51 passing signal

52 reflected signal

5 DETAILED DESCRIPTION OF PREFERRED EMBODIMENT

An embodiment of the present invention will be described as follows with drawings.

Fig. 1 is a block diagram showing the structure of a communication device including an antenna switch module of the
 10 embodiment of the present invention. In Fig. 1, a communication device includes antenna switch module 30, transmission part 41, reception part 42, filter 43, antennas 44 and 45, and capacitors C11 to C14. Antenna switch module 30 includes antenna switch 33, filter 31 and adjustment line 13D. Adjustment line 13D,
 15 together with other components described later, make up directional coupler 35.

Signals from transmission part 41 are inputted to filter 31 through capacitor C11. Filter 31 is a notch low pass filter which removes unnecessary harmonic signals contained in the
 20 signals from transmission part 41. Filter 31 has fundamental frequencies of 4.9 to 5.85 GHz. The second harmonic frequencies are from 9.8 to 11.7 GHz, and the third harmonic frequencies are from 14.7 to 17.55 GHz. Signals outputted from filter 31 are inputted to antenna switch circuit 33 through adjustment
 25 line 13D made of stripline. The signals inputted through adjustment line 13D are emitted from antenna 44 or 45 selected by antenna switch circuit 33, after passing through capacitor C13 or C14.

On the other hand, signals received by antenna 44 or 45

selected by antenna switch circuit 33 through capacitor C13 or C14 are inputted to filter 43 through capacitor C12. Filter 43 removes unnecessary signals from the received signals, and outputs them to reception part 42. Reception part 42
 5 demodulates the signals from filter 43.

Figs. 2 to 7 show the respective layers of a multilayer substrate in the case where the antenna switch module of the present embodiment is compliant with IEEE802.11a. Fig. 2 shows first layer P1, which is the uppermost layer. First layer P1
 10 is provided thereon with switching element B1, inductors L1 to L4, capacitors C1, C2 and resistors R1, R2 so as to form antenna switch circuit 33. Switching element B1 is made up of PIN diodes D1 to D4. First layer P1 is further provided thereon with capacitor C12, filter 43, and capacitor C5 and resistor R5 which
 15 are components of directional coupler 35.

Fig. 3 shows second layer P2 having ground parts 5A and 5B thereon. Fig. 4 shows third layer P3 having coupling line 15 thereon, which is a component of the directional coupler. Fig. 5 shows fourth layer P4 having filter 31 and adjustment
 20 line 13D thereon. Fig. 6 shows fifth layer P5 having ground part 4 thereon. Fig. 7 shows sixth layer P6 provided thereon with electrodes 6A to 6E. With layer P1 as the uppermost layer, layers P2 to P6 are arranged from above in this order. The antenna switch module of the present embodiment is connected with another
 25 device via P6.

The substrate of the antenna switch module of the present embodiment is made from low-temperature co-fired ceramics having a dielectric constant of 7.4, and is 5.4 mm by 4.0 mm and 0.7 mm in thickness. Ground parts 4, 5A and 5B; striplines

11A to 11D and 13A to 13C; adjustment line 13D; and coupling line 15 are formed by printing conductive paste mainly composed of silver powder.

In the present embodiment, striplines 11A to 11D, 13A to
5 13C and adjustment line 13D formed on the fourth layer have a characteristic impedance of 50 ohms, and a line width of 0.1 mm in the case of the low-temperature co-fired ceramics of the present embodiment. Filter 31 is made up of striplines 11A to 11D and 13A to 13C. Stripline 11A is connected with striplines
10 13A and 13B at junction point E1. Stripline 11B and 11C are connected with striplines 13B and 13C at junction point E2.

Stripline 11D is connected with stripline 13C and adjustment line 13D at junction point E3. In order to reduce the size of filter 31, striplines 11B, 11C, 13B and 13C are
15 connected in the shape of a cross at junction point E2. Striplines 11A to 11D are open at one side, and have line lengths of $1/4$ wavelengths of 17.55 GHz, 14.7 GHz, 11.7 GHz and 9.8 GHz, respectively. Consequently, striplines 11A, 11B, 11C and 11D have a voltage swing of 0 at junction points E1 to E3 at 17.55
20 GHz, 14.7 GHz, 11.7 GHz and 9.8 GHz, respectively. In other words, striplines 11A to 11D are open stubs.

These striplines are bent to reduce the filter size, while keeping an interval long enough not to cause line coupling. In this embodiment, the line interval is made to be not less than
25 0.15 mm. Filter 31 may be made up of, instead of the $1/4$ wavelength open stubs, $1/2$ wavelength short stubs whose each one side is grounded. In this case, it is necessary to insert a DC cut capacitor between filter 31 and antenna switch circuit 33.

The line lengths of striplines 13B and 13C are determined in such a manner that in the condition where striplines 11A to 11D are connected with each other, the impedance when junction point E1 is seen from the stripline 13A side and the impedance
5 when junction point E3 is seen from adjustment line 13D can be 50 ohms at the fundamental frequencies. For example, in the case of the low-temperature co-fired ceramics of the present embodiment, striplines 13B and 13C have line lengths of 2.3 mm and 2.45 mm, respectively.

10 Stripline 13A is connected to round conductor 3. The fourth and fifth layers are connected with each other through via hole V1. The fifth layer is connected with electrode 6A on the sixth layer through via hole V2. Round conductor 8 connects between via holes V1 and V2. Electrode 6A on the sixth layer
15 is connected with transmission part 41 through C11.

On ground part 4, part of the conductor pattern is cut in the form of a circle with a diameter not to cause electromagnetic coupling due to via hole V2. In the present embodiment, round conductor 8 has a diameter of 1.25 mm, and
20 a via hole diameter of 0.5 mm. Round conductor 3 has a diameter of 0.75 mm in consideration of positional deviation or positional variation between round conductor 3 and the via hole due to manufacturing errors.

On the sixth layer, electrodes 6A to 6E are formed by
25 printing conductive paste mainly composed of silver powder. Electrode 6A receives signals from transmission part 41 through capacitor C11. Electrodes 6C and 6D supply power to operate antenna switch circuit 33. A plurality of electrodes 6E assure a ground potential. The round electrode on the sixth layer has

a diameter of 1 mm. In order to fix the potential of ground part 4 on the fifth layer, electrodes 6B, which are rectangles of 0.8 mm by 1.4 mm, are formed at the positions of ± 0.7 mm from the center of the sixth layer in such a manner as to be symmetric
 5 with respect to the center. Electrodes 6B each include via holes, which are arranged in two columns and five rows at an interval of 0.3 mm by 0.5 mm, and are connected with ground part 4.

Adjustment line 13D is connected with round conductor 7, and is further connected with terminal T1 of antenna switch
 10 circuit 33 shown in Fig. 2 through via hole V3 connecting between the fourth and second layers, and via hole V4 connecting between the second layer and antenna switch circuit 33.

Fig. 8 shows the structure of antenna switch circuit 33 of the antenna switch module of the present embodiment. In Fig.
 15 8, antenna switch circuit 33 includes terminals T1 to T4. Terminal T1 receives signals from transmission part 41. Terminal T2 outputs signals from antenna 44 or 45 to reception part 42. Terminal T3 is connected with antenna 44 through capacitor C13. Terminal T4 is connected with antenna 45 through
 20 capacitor C14. Antenna switch circuit 33 is provided with switch units S1 and S2. Switch unit S1 electrically connects/disconnects terminal T1 and terminals T3, T4. Switch unit S2 electrically connects/disconnects terminal T2 and terminals T3, T4.

25 Switch unit S1 includes PIN diode D1 connecting between terminal T1 and the cathode and between terminal T3 and the anode, and PIN diode D2 connecting between terminal T1 and the anode and between terminal T4 and the cathode. Switch unit S2 includes PIN diode D3 connecting between terminal T2 and the anode and

between terminal T3 and the cathode, and PIN diode D4 connecting between terminal T2 and the cathode and between terminal T4 and the anode. PIN diodes D1 to D4 make up switching element B1.

Inductor L1 and capacitor C1 are connected in series with
 5 each other between ground 5B and the junction point of terminal T1 and PIN diode D1. Inductor L2 and capacitor C2 are connected in series with each other between ground 5B and the junction point of PIN diode D1 and terminal T3. Inductor L3 and capacitor C1 are connected in series with each other between ground 5B
 10 and the junction point of terminal T2 and PIN diode D4.

Inductor L4 and capacitor C2 are connected in series with each other between ground 5B and the junction point of PIN diode D4 and terminal T4. The junction point of inductors L1, L3 and capacitor C1 is connected with electrode 6C through resistor
 15 R1. The junction point of inductors L2, L4 and capacitor C2 is connected with electrode 6D through resistor R2.

Resistors R1 and R2 control the direct currents flowing to PIN diodes D1 to D4. Capacitors C1 and C2 bypass high frequency components to ground 5B. Inductors L1 to L4 block the
 20 high frequency components and supply direct current voltages to PIN diodes D1 to D4. Supplying a positive direct-current voltage to electrode 6C makes PIN diodes D2 and D3 "ON". Supplying a positive direct-current voltage to electrode 6D makes PIN diodes D1 and D4 "ON".

25 Fig. 9 is an equivalent circuit diagram when a PIN diode as a component of the antenna switch circuit of the present embodiment is "ON", and the PIN diode is made up of inductors L31 to 33, capacitor C31 and resistor 31. Fig. 10 is an equivalent circuit diagram when the PIN diode of the present

embodiment is "OFF", and the PIN diode is made up of inductors L34 and L35, capacitors C32 and C33, and resistor 32. In Fig. 4, coupling line 15, together with capacitor C5 and resistor R5, makes up directional coupler 35 by being in parallel with adjustment line 13D via the ceramics layer.

The operation of the antenna switch module of the present embodiment thus structured will be described as follows.

Fig. 11 shows frequency characteristics of the antenna switch module of the present embodiment. Passing signal 51 is passed from stripline 13A to terminal T3 or T4. Reflected signal 52 is a reflected signal corresponding to passing signal 51. In antenna switch circuit 33, the impedance when terminal T3 connected with capacitor C13 is seen from terminal T1 connected with adjustment line 13D is referred to with Z_{13} . The impedance when terminal T2 connected with capacitor C12 is seen from terminal T4 connected with capacitor C14 is referred to with Z_{42} . The impedance when terminal T4 is seen from terminal T1 is referred to with Z_{14} . The impedance when terminal T2 is seen from terminal T3 is referred to with Z_{32} .

As shown in Fig. 11, filter 31 formed on the fourth layer produces large attenuation poles with striplines 11A to 11D at the frequencies which are the second and third harmonics of the fundamental frequencies ranging from 4.9 GHz to 5.85 GHz. Furthermore, the length of adjustment line 13D made up of the striplines is controlled so as to prevent the impedance Z_{13} when stripline 13A is seen from round conductor 7 at the second and third harmonic frequencies and the impedance Z_{14} when antenna switch circuit 33 is seen from round conductor 7 from becoming complex conjugates of each other. In other words, impedances

Z13 and Z14 are prevented from having an equal resistance component, and reactance components equal in size and opposite in sign.

The following is a more detailed description. Antenna
5 switch circuit 33, which operates properly as a switch at the
fundamental frequencies ranging from 4.9 GHz to 5.85 GHz, does
not operate properly as a switch at frequencies of the second
and higher harmonics of the fundamental frequencies. This is
due to the influence of the reactance component shown in Figs.
10 9 and 10. This situation is dealt with as follows. Measured
data of antenna switch circuit 33 are inputted to an EM
(electromagnetic) simulator. Next, the specifications of
filter 31 made from low-temperature co-fired ceramics, that is,
the actual layer structure and detailed requirements of the
15 conductors such as conductor loss are inputted to the EM
simulator. In the same manner, the specifications of adjustment
line 13D, that is, the actual layer structure and detailed
requirements of the conductors such as conductor loss are
inputted to the EM simulator. The length of adjustment line 13D
20 is changed to avoid a complex conjugate relation at the second
and third harmonics, thereby obtaining favorable amount of
attenuation and band width.

By using a notch low pass filter as the filter and
controlling the length of adjustment line 13D, an antenna switch
25 module can be provided which reduces filtering loss so as to
ensure high attenuation in a wide band at harmonic frequencies.

The directional coupler can be alternatively made up of
adjustment line 13D, coupling line 15, capacitor C5 and resistor
R5. This allows more reflected waves to be detected from antenna

44 or 45, thereby controlling the transmission condition of transmission part 41.

As described hereinbefore, the antenna switch module of the present invention can easily reduce rebound components
5 between two or more attenuation poles of the filter without degrading the amount of attenuation at the attenuation poles, thereby fully attenuating the harmonic components without increasing the number of stages of the filter.

In the present embodiment, it is alternatively possible
10 to divide the ground part into ground part 5A and ground part 5B. Ground part 5A is for antenna switch circuit 33. Ground part 5B is for striplines 13B to 13C and 11A to 11D composing the filter on the fourth layer, and stripline 13A and round conductor 3 which are connected to transmission part 41.

15 This division of the ground allows the image current to flow through ground part 5A, and then into ground part 4 through via hole V5 connecting between ground part 5A and ground part 4.

Then, the image current flowing through ground part 4 is
20 flown into ground part 5B through via hole V6 connecting between ground part 4 and ground part 5B. The path of the image current has a considerable line length at the second and higher harmonic frequencies of the fundamental frequencies ranging from 4.9 GHz to 5.85 GHz. In other words, the image current path functions
25 as a choke coil for the current at the second and higher harmonic frequencies. As a result, in these frequencies, the antenna switch module of the present embodiment can obtain favorable amount of attenuation of 30 dB or higher.

The present embodiment takes up the case where the

switching element of the antenna switch circuit is a PIN diode with excellent switch properties at high frequencies; however, the present invention is not limited to this case. Equivalent effects could be obtained by using as the switching element other
5 electronic devices such as Ga(gallium)As(arsenic) switches having favorable switch properties at high frequencies, transistors, and electric field-effect transistors (FETs).

The filter or the adjustment line, which is formed of striplines in the present embodiment, could be formed of
10 microstriplines to obtain the equivalent effects. Although four attenuation poles are used in the present embodiment, the number can be other than four. The filter, which is a notch low pass filter in the present embodiment, could be a polarized low pass filter to obtain the equivalent effects.

15 The filter, which is a low pass filter in the present embodiment, could be a band pass filter or a band rejection filter to obtain the equivalent effects. Although the multilayer substrate consists of six layers in the present embodiment, the number can be other than six.

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INDUSTRIAL APPLICABILITY

As described hereinbefore, the antenna switch module of the present invention includes a filter which reduces transmission loss so as to achieve high attenuation in a wide
25 band at harmonic frequencies and an adjustment line. Therefore, this is useful as an antenna switch module or the like including an antenna switch to switch antennas and a filter to remove spurious signals from the communication device.